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# A Theoretical Comparison of the Near-Optimum Design and Predicted Performance of n/p and p/n Indium Phosphide Homojunction Solar Cells

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#### **ABSTRACT**

Using our detailed simulation model of p<sup>+</sup>nn<sup>+</sup> and n<sup>+</sup>pp<sup>+</sup> Indium Phosphide (InP) homojunction solar cells, we have done extensive parametric variation computer simulation runs to help us arrive at near-optimum designs of these two solar cell configurations. In this paper, we present the values of all the geometrical and material parameters corresponding to the near-optimal designs of both these configurations. Next, for each configuration, we present the results of parametric variation runs showing how the performance parameters  $J_{sc}$ ,  $V_{oc}$  and  $\eta$  vary with each of the cell design parameters for the near-optimally designed cell. Finally, we discuss the theoretical results obtained and compare the relative merits and drawbacks of the two configurations.

## INTRODUCTION

In recent years, in laboratory irradiation tests, indium phosphide (InP) homojunction solar cells have shown a markedly higher tolerance to 1 MeV electron and 10 MeV proton irradiation than silicon (Si) and gallium arsenide (GaAs) solar cells [1]; this fact makes indium phosphide solar cells very attractive for space applications [2]. The main task in the design of InP solar cells is, then, to design them as to yield the maximum possible beginning-of-life (BOL) energy conversion efficiency, comparable to, or greater than that obtained from gallium arsenide solar cells ( $\approx$ 22% at AMO, 25°C).

Using a fairly complete computer simulation model of the homojunction InP solar cell [3], we have done an extensive parameter variation study which has allowed us to come up with near-optimum designs of the InP homojunction solar cell in both its  $n^{\dagger}pp^{\dagger}$  (n-on-p) and  $p^{\dagger}nn^{\dagger}$ 

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(p-on-n) configurations. Having obtained the near-optimum designs of the two configurations, we then re-did the parameter variation study such that while each parameter was being varied individually, all other parameters were kept fixed at their near-optimum values. It is the results of such a parameter variation study of the near-optimum cell design that we present in this paper. While so doing we also compare the theoretically predicted performance of near-optimally designed  $n^{\dagger}pp^{\dagger}$ and p<sup>+</sup>nn<sup>+</sup> (p-on-n) InP homojunction space solar cell configurations. Such a comparison is necessary and useful since, there is no a priori reason why a particular one of these two configurations should have the higher beginning-of-life (BOL) efficiency. In addition, we had shown in an earlier paper [4], that the primary factor limiting the open circuit voltage and efficiency of the n'pp' InP homojunction solar cell is the relatively large heavy doping factor in the heavily doped p back-surface field (BSF) region and had mentioned there that since the heavy doping factor in heavily doped n-type InP is quite likely much smaller than that in p-type InP, it was worth investigating the BOL performance of the near-optimally designed  $p^{\dagger}nn^{\dagger}$  InP solar cell.

#### RESULTS AND DISCUSSION

# A. Near-Optimum Designs

Table 1 gives the geometrical, material and performance parameters of the near-optimum designs of the  $n^+pp^+$  and  $p^+nn^+$  (p-on-n) homojunction InP solar cell configurations. In this table, the values of the minority carrier indirect or Hall-Shockley-Reed lifetime coefficients in n- and ptype InP are assumed to be ten times the values obtained by matching (curve-fitting) the measured curves of illuminated I-V,  $\log_{10}I_{sc}$  versus  $V_{oc}$ and spectral response, to the corresponding calculated curves, for an  $n^{\dagger}pp^{\dagger}$  homojunction InP solar cell made by the Spire Corporation (Cell Spire 6 [5]). This is along the same lines as we have done earlier [4] As indicated in the table, the heavy doping factors in the various regions were also obtained by matching the calculated and measured curves for the above measurements for the Spire 6 solar cell. The minority carrier mobilities and diffusivities in the various regions were obtained in the same manner as we have explained before [3]. The design parameters, namely, the thickness of and doping in each cell region were obtained from an extensive parametric variation study and are those values which yield the maximum efficiency.

In comparing the  $n^{\dagger}pp^{\dagger}$  and  $p^{\dagger}nn^{\dagger}$  near-optimum cell designs, note the considerable difference in the emitter thickness of configurations. Because of the significantly higher electron mobility compared to hole mobility in InP, the minority carrier diffusion length is much longer in p-type InP than in n-type InP. Hence, it is advantageous to have most of the incoming photons be absorbed in the ptype InP, regardless of configuration. This means that the p-region should be as close to the surface as possible and should be wide enough to absorb most of the incoming photons. This is achieved by choosing either the  $p^{\dagger}nn^{\dagger}$  configuration with a wide emitter or the  $n^{\dagger}pp^{\dagger}$ configuration with a thin emitter. An immediate implication of this fact is that a larger fraction of the short circuit current  $\mathbf{I}_{\text{sc}}$  comes from the emitter in the  $p^+nn^+$  configuration compared to that in the  $n^+pp^+$ 

Table 1 Geometrical, Material and Performance Parameters of Near-Optimum n\*pp\* and p\*nn\* Homojunction Indium Phosphide Solar Cells.

## a) n\*pp\* Structure

Grid Shadow	4.0%
Front SRV	1 x 10 <sup>4</sup> cm/sec
$W_{\scriptscriptstyle m E}$	200 Å
N <sub>D,emitter</sub>	$3 \times 10^{18} \text{ cm}^{-3}$
$^{\bullet} HD_{E} = n_{iE} / n_{iO}$	0.837
· T <sub>HSR</sub>	6.667 ns
T <sub>Rad</sub>	0.469 ns
$\tau_{p,E}$	0.437 ns
$L_{p,\mathbb{E}}$	0.229 μm
$W_{ m base}$	4.0 μm
N <sub>A,base</sub>	$8 \times 10^{15} \text{ cm}^{-3}$
HD <sub>base</sub>	1.0
* T <sub>HSR</sub>	3.750 µs
T <sub>Rad</sub>	0.176 μs
T <sub>n,B</sub>	0.168 µs
$L_{n,\mathrm{base}}$	43.29 μm
$W_{\mathtt{BSF}}$	250 μm
N <sub>A,BSF</sub>	7.5 x 10 <sup>16</sup> cm <sup>-3</sup>
HD <sub>BSF</sub>	1.0
· τ <sub>HSR</sub>	400 ns
τ <sub>Rad</sub>	18.74 ns
T <sub>n,BSF</sub>	17.89 ns
$L_{n,\mathrm{BSF}}$	12.45 μm

*	Quantities	obtained	from	Spire	6	match.

$J_{SC}$	$= 39.94 \text{ mA} / \text{cm}^2$
$V_{oc}$	= 901.3  mV
$J_{max}$	$= 38.57 \text{ mA} / \text{cm}^2$
Vmax	= 804.4  mV
FF	= 86.21 %
n	= 22.60 %

## b) p\*nn\* Structure

Grid Shadow	4.0%
Front SRV	1 x 10 <sup>3</sup> cm/sec
$W_{\mathtt{E}}$	3500 Å
N <sub>A,emitter</sub>	$1 \times 10^{18} \text{ cm}^{-3}$
$^{\bullet} HD_E = n_{iE} / n_{iO}$	3.0
T <sub>HSR</sub>	30 ns
T <sub>Rad</sub>	1.406 ns
τ <sub>n,E</sub>	1.327 ns
$L_{n,\mathrm{E}}$	2.971 µm
$W_{ m base}$	3.0 µm
	1 x 10 <sup>16</sup> cm <sup>-3</sup>
$N_{D,\mathrm{base}} \ \mathrm{HD}_{\mathrm{base}}$	1.0
τ <sub>HSR</sub>	2.0 μs
	140.6 ns
τ <sub>Rad</sub>	131.3 ns
$ au_{p,\mathrm{B}} \ L_{p,\mathrm{base}}$	7.349 µm
	200
$W_{\mathtt{BSF}}$	300 μm
$N_{D, \mathrm{BSF}}$	$5.0 \times 10^{18} \text{ cm}^{-3}$
HD <sub>BSF</sub>	1.0
• τ <sub>HSR</sub>	4.0 ns
$ au_{ ext{Rad}}$	0.281 ns
$ au_{p, exttt{BSF}}$	0.249 ns
$L_{p, \mathrm{BSF}}$	0.152 μm

\* Quantities obtained from Spire 6 match.

 $J_{SC}$  = 39.65 mA / cm<sup>2</sup>  $V_{OC}$  = 915.3 mV  $J_{max}$  = 38.32 mA / cm<sup>2</sup>  $V_{max}$  = 808.5 mV FF = 85.35 %  $\eta$  = 22.56 %

configuration, as shown in Table II. This table gives, for the  $n^{\dagger}pp^{\dagger}$  and  $p^{\dagger}nn^{\dagger}$  configurations, the components of the short circuit current density  $J_{sc}$  from each of the emitter, space charge and base regions, both in terms of  $mA/cm^2$  and as fractions of the total current density. Note that in the  $p^{\dagger}nn^{\dagger}$  configuration, over 92% of the short circuit current  $I_{sc}$  comes from the emitter and space charge regions while in the  $n^{\dagger}pp^{\dagger}$  configuration, only 30.5% of  $I_{sc}$  comes from these regions. This fact has strong implications on the radiation damage in these two configurations. For a radiation environment in which the radiation-induced defect creation in the InP material occurs primarily at a depth  $\geq 1~\mu m$ , the  $p^{\dagger}nn^{\dagger}$  structure will suffer very little degradation of its  $I_{sc}$  compared to the  $n^{\dagger}pp^{\dagger}$  structure for which about 70% of its  $I_{sc}$  comes from deeper in the base region. For a radiation environment in which defect creation in the InP

material occurs close to the surface ( $\leq$  1  $\mu\text{m}),$  the  $\text{p}^{\scriptscriptstyle{\dagger}}\text{nn}^{\scriptscriptstyle{\dagger}}$  structure will suffer more degradation of its  $\mathbf{I}_{sc}$  than the  $\mathbf{n}^t\mathbf{p}\mathbf{p}^t$  structure.

Table 2 Fractions of Isc coming from various regions of near-optimally designed n/p and p/n solar cells.

	Emitter	SCR	Base	Total
n/p	6.36 15.9 %	5.83 14.6 %	27.74 69.6 %	39.94 mA/cm <sup>2</sup> 100 %
p/n	31.6 79.7 %	4.97 12.5 %	3.06 7.72 %	39.65 mA/cm <sup>2</sup> 100 %

Ιn comparing beginning-of-life (BOL) performance of the nearoptimum designs of the n<sup>+</sup>pp<sup>+</sup> and p<sup>+</sup>nn<sup>+</sup> solar cell configurations, we see from Table I that the near-optimum designs of both the n'pp' and p<sup>t</sup>nn<sup>t</sup> configurations capable οf yielding essentially the same 1 AMO 25°C efficiency of slightly over 22.5%. The

configuration has a somewhat higher  $V_{\text{oc}}$  but somewhat lower  $J_{\text{sc}}$  and FF than the n<sup>+</sup>pp<sup>+</sup> configuration.

# B. Parametric Variation Study

1a

1) Front Surface Recombination Velocity S<sub>F</sub>.

Figures la,b,c show. respectively, the  $J_{sc}\text{, }V_{oc}$  and  $\eta$  of  $n^{\dagger}pp^{\dagger}$  and  $p^{\dagger}nn^{\dagger}$  near-optimum InP solar cells as functions of the front surface recombination velocity  $S_{\rm F}$ . Note that all performance parameters,  $J_{sc}$ , degrade heavily increasing  $S_{\scriptscriptstyle F}$  in the upper ranges of  $S_{F}$ for only the p<sup>†</sup>nn<sup>†</sup> configuration. The performance

Fig. Current Density  $J_{sc}$  of Near-Optimum Cell vs. front SRV S (mA/cm²) 40

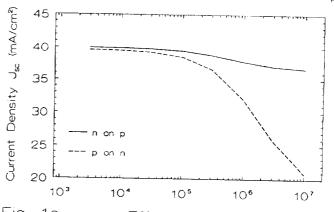
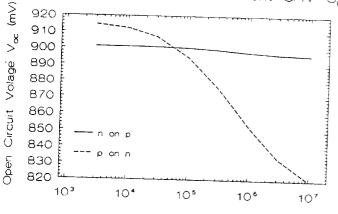
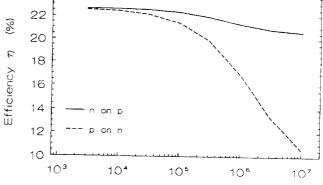


Fig. 1b Open Circuit Voltage of Fig. 1c Efficiency  $\eta$  of Near-Optimum Cell vs. front SRV  $S_{\rm E}$ Near-Optimum Cell vs. front SRV



10  $10^{3}$ 104 105 106 Front Surface Recomb Velocity (cm/s)

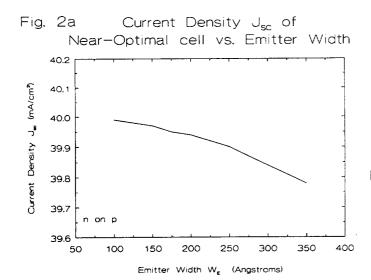
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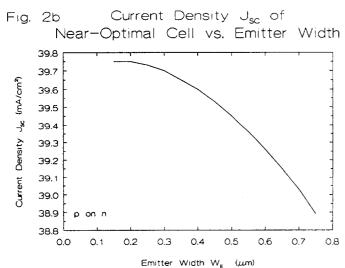


Front Surface Recomb Velocity (cm/s)

degradation is relatively minor for the  $n^+pp^+$  configuration even at  $S_F$  values approaching its limiting value of  $v_{th}/2 \sim 10^7$  cm/s. This grossly different dependence on  $S_F$  for the  $n^+pp^+$  and  $p^+nn^+$  configurations is easy to explain if we consider that because of its substantially thicker emitter, the  $p^+nn^+$  configuration has most of its photocurrent coming from the emitter and this makes the  $p^+nn^+$  configuration much more sensitive to all the emitter parameters (front SRV, emitter doping, emitter thickness etc.) than the  $n^+pp^+$  configuration.

## 2) Emitter Thickness W<sub>E</sub>.





 $V_{oc}$ and η parameters,  $J_{sc}$ , 2%, as less than emitter thickness varies from 100Å to 350Å for the  $n^{\dagger}pp^{\dagger}$  and from 0.1 μm for 0.75 the µm to Note also that all configuration. the three performance parameters  $J_{sc}$ ,  $V_{oc}$  and  $\eta$  initially increase the monotonically as

2a,b Figures respectively, the  $J_{sc}$  for the  $n^{+}pp^{+}$ p<sup>+</sup>nn<sup>+</sup> configurations Figures 2c,d show the  $V_{oc}$  and  $oldsymbol{\eta}$  for the same two configurations, all emitter functions of the thickness  $W_E$ . Here, note that for and n<sup>†</sup>pp<sup>†</sup> the performance configurations, all

Fig. 2c Open Circuit Voltage & Efficiency of Near Optimal cell vs. Emitter Width

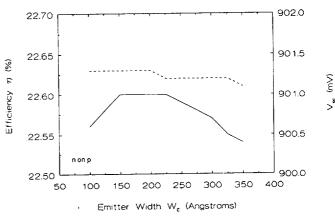
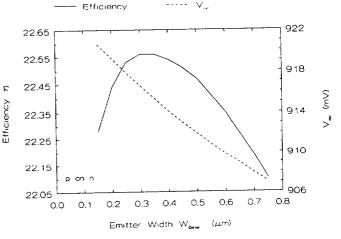
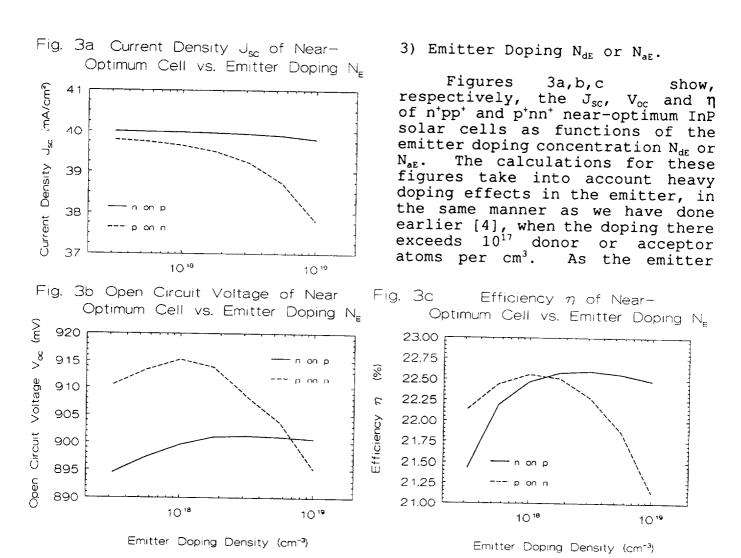


Fig. 2d Open Circuit Voltage & Efficiency of Near Optimal cell vs. Emitter Width



thickness  $W_E$  decreases. While this trend holds for  $J_{SC}$  and  $V_{OC}$  all the way down to  $W_E$  = 100Å for the n<sup>†</sup>pp<sup>†</sup> configuration and  $W_E$  = 0.1 $\mu$ m for the p<sup>†</sup>nn<sup>†</sup> structure, the curve for  $\eta$  peaks in the range of  $W_E$  between 150Å and 225Å for the n<sup>†</sup>pp<sup>†</sup> and  $W_E$  between 0.3 and 0.4  $\mu$ m for the p<sup>†</sup>nn<sup>†</sup> structure. For  $W_E$  shorter than the lower limits of these ranges, the efficiency  $\eta$  decreases with further decreases in  $W_E$ . This is because in these ranges of  $W_E$  values, the overall series resistance of the solar cell is dominated by the emitter sheet resistance which increases with decreasing  $W_E$ , causing the fill factor FF and thereby also the efficiency  $\eta$  to decrease with decreasing  $W_E$ . Thus for both the n<sup>†</sup>pp<sup>†</sup> and p<sup>†</sup>nn<sup>†</sup> configurations, there is an optimum range of values of  $W_E$ , which yield the highest efficiency. For the n<sup>†</sup>pp<sup>†</sup> structure this optimum range of  $W_E$  is from ~150Å to ~225Å, while for the p<sup>†</sup>nn<sup>†</sup> structure, the optimum range of  $W_E$  is 0.25-0.425  $\mu$ m.



doping increases from  $10^{17}$  to  $10^{19}$  cm<sup>-3</sup>, two detrimental effects come into play. First, the radiative lifetime in the emitter decreases in inverse proportionality to the doping increase and secondly, the effective bandgap narrowing significantly increases the effective intrinsic carrier

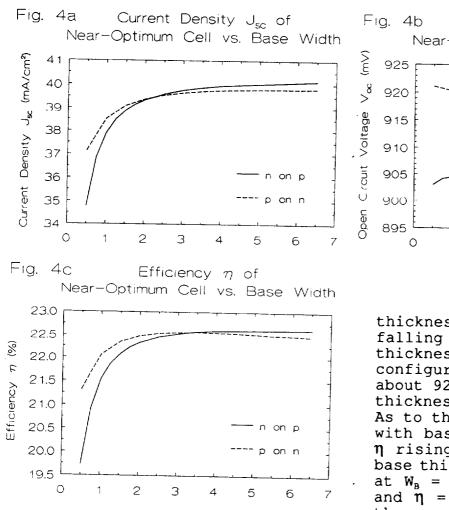
concentration, thereby increasing the dark saturation or loss current. Of these, it is primarily the first effect, namely, the reduction of lifetime, which is responsible for the degradation of  $J_{sc}$  with increased emitter doping. However, both detrimental effects affect  $V_{oc}$  and cause it to degrade with increasing doping.

Here, in comparing the n<sup>†</sup>pp<sup>†</sup> and p<sup>†</sup>nn<sup>†</sup> configurations, we see that the n<sup>†</sup>pp<sup>†</sup> cell suffers only a ~0.6% drop in its  $J_{sc}$  as the emitter doping increases from  $10^{17}$  to  $10^{19}$  cm<sup>-3</sup> while the p<sup>†</sup>nn<sup>†</sup> cell suffers a 5.12% reduction in its  $J_{sc}$  over the same range of emitter doping increase. This difference in behavior is easily explained, knowing that in the p<sup>†</sup>nn<sup>†</sup> structure about 80% of the  $J_{sc}$  comes from the emitter as compared to only about 16% from the emitter for the n<sup>†</sup>pp<sup>†</sup> structure. Thus, as the minority carrier lifetime and diffusion length in the emitter reduce with increased doping in that region, a larger current is affected in the p<sup>†</sup>nn<sup>†</sup> structure than in the n<sup>†</sup>pp<sup>†</sup> structure, giving a larger amount of degradation in the p<sup>†</sup>nn<sup>†</sup> compared to the n<sup>†</sup>pp<sup>†</sup> structure.

As to the variation of  $V_{oc}$  and  $\eta$  with emitter doping, we see a somewhat different behavior between the  $n^tpp^t$  and  $p^tnn^t$  structures. For the  $\ensuremath{\text{n}^{\scriptscriptstyle +}}\xspace pp^{\scriptscriptstyle +}\xspace$  , both  $\ensuremath{\text{V}_{\text{oc}}}\xspace$  and  $\eta$  first rapidly increase with increasing emitter doping, and then very very gradually decrease with further increases in emitter doping. For the p<sup>+</sup>nn<sup>+</sup> cell,  $V_{oc}$  first decreases, reaches a minimum at an emitter doping of  $3*10^{17}$  cm<sup>-3</sup>, then increases, reaches a maximum, and then decreases continually up to an emitter doping of  $10^{19}~\text{cm}^{-3}$ . The observed behavior of  $V_{\text{oc}}$  versus emitter doping is explainable by considering the fact that in p-type InP, heavy doping causes a increase in nie, the effective intrinsic substantial concentration, thereby increasing the loss current (dark saturation current) and reducing  $V_{oc}$  [4]. In n-type InP, heavy doping causes the bandgap to widen rather than become narrow [4]. Therefore,  $n_i$  either reduces or, at worst, stays the same. Thus, for the n'pp' cell, there is no degradation of  $V_{\text{oc}}$  due to heavy doping effects and the rather slight reduction of  $V_{\text{oc}}$  with increasing emitter doping seen in Figure 3b is due to the reduction of the minority carrier lifetime in the emitter with increasing doping there. For the  $p^{\dagger}nn^{\dagger}$  cell, at emitter dopings higher than  $\sim 10^{18} \, \text{cm}^{-3}$ ,  $V_{\text{oc}}$  decreases with increasing emitter doping due to both, the heavy doping factor and the reduction in lifetime. Hence, a much steeper decline in  $V_{\text{oc}}$  with increasing emitter doping is seen for the p<sup>+</sup>nn<sup>+</sup> structure as compared to the ntppt structure.

# 4) Base Width W<sub>B</sub>

Figures 4 a,b,c show, respectively, the  $J_{sc},$   $V_{oc}$  and  $\eta$  of  $n^{+}pp^{+}$  and  $p^{+}nn^{+}$  InP homojunction solar cells as functions of the base thickness  $W_{B}.$  First considering figure 4a, we see that  $J_{sc}$  increases monotonically with base thickness for both the  $n^{+}pp^{+}$  and  $p^{+}nn^{+}$  configurations and substrates at a value of slightly below 40 mA/cm² at a base thickness of about  $4\mu m.$  In this regard, both the  $n^{+}pp^{+}$  and  $p^{+}nn^{+}$  configurations behave similarly and there is no unexpected behavior anywhere. Figure 4b,c show the  $V_{oc}$  and  $\eta$  of the two configurations as functions of the base thickness. In comparing the two configurations with respect to their  $V_{oc}$  as a function of base thickness, we note that the  $n^{+}pp^{+}$  cell shows  $V_{oc}$  initially rising with increasing base thickness, reaching a maximum of about 905 mV at a



Base Width (um) thickness of about  $1\mu m$  and then falling with increasing thickness. For the p<sup>+</sup>nn<sup>+</sup> configuration, the maximum  $\boldsymbol{V}_{\text{oc}}$  is about 921 mV and occurs at a base thickness of approximately  $0.5\mu m$ . As to the variation of efficiency with base width, figure 4c shows  $\eta$  rising rapidly with increasing base thickness, reaching  $\eta = 19.7$ % at  $W_B = 0.5 \mu m$ , for the  $n^+pp^+$  cell and  $\eta = 21.3\%$  at  $W_B = 0.5\mu m$  for p<sup>†</sup>nn<sup>†</sup> cell.

configurations saturate to 1AMO, 25°C  $\eta$  of very close to 22.5% for

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Open Circuit Voltage of

Near-Optimum Cell vs. Base Width

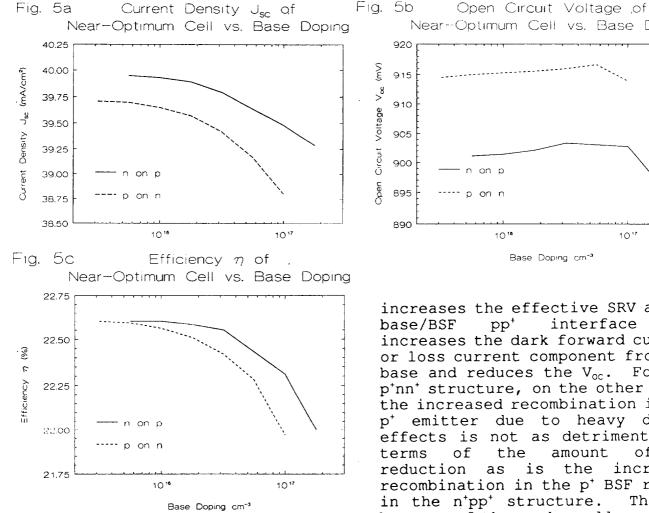
base thickness greater than  $\sim 3.5 \mu m$ .

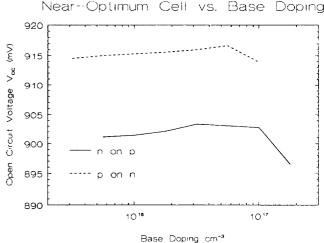
Base Width (µm)

# 5) Base Doping $N_{aB}$ or $N_{dB}$ .

Figures 5a,b,c show, respectively, the  $J_{\text{SC}}$ ,  $V_{\text{OC}}$  and  $\eta$  of n\*pp\* and p\*nn\* InP homojunction solar cells as functions of the base doping  $N_{\text{aB}}$  or  $N_{\text{dB}}$ . First, considering figure 5a, we see that the  $J_{\text{SC}}$  of the n\*pp\* device is slightly but consistently higher than  $J_{\text{SC}}$  of the p\*nn\* device. This difference is due to the fact that most of the photogenerated carriers in the p\*nn\* cell come from the emitter where, because of the heavier doping needed to reduce the sheet resistance to a reasonable value, the minority carrier lifetime is shorter and the collection efficiency of these photogenerated carriers is poorer than in the less heavily doped base region, where most of the photocurrent comes from for the n\*pp\* cell.

Next, looking at figure 5b, which shows  $V_{oc}$  versus base doping, we see that the  $V_{oc}$  of the p<sup>+</sup>nn<sup>+</sup> near-optimum cell is consistently higher than that of the near-optimum n<sup>+</sup>pp<sup>+</sup> cell. This is explainable on the basis that heavy doping effects play a detrimental role only in p-type InP. Then, for the n<sup>+</sup>pp<sup>+</sup> structure, the increased recombination in the p<sup>+</sup> BSF





increases the effective SRV at the base/BSF ppt interface increases the dark forward current or loss current component from the base and reduces the  $V_{oc}$ . For the p'nn' structure, on the other hand, the increased recombination in the p<sup>+</sup> emitter due to heavy doping effects is not as detrimental in of terms the amount of reduction as is the increased recombination in the  $p^+$  BSF region in the n<sup>+</sup>pp<sup>+</sup> structure. because of the much smaller volume of the emitter, with its thickness

of only 400Å, compared to the volume of the BSF region, with its thickness of  $> 10 \mu m$ .

Finally, looking at figure 5c, showing  $\eta$  as a function of base doping for both structures, we see that for a base doping less than ~ 5\*10<sup>15</sup> cm<sup>-3</sup>, both near-optimum structures have the same efficiency of 22.6% at 1AMO, 25°C. However, as the base doping increases, the n<sup>+</sup>pp<sup>+</sup> structure starts showing a higher  $\eta$  than the p<sup>+</sup>nn<sup>+</sup> structure and the difference in η between the two structures keeps widening with increasing base doping.

#### CONCLUDING REMARKS

From Table 1 as well as the figures showing the efficiency  $\eta$  versus any of the parameters, we see that the near-optimal designs of both the n<sup>†</sup>pp<sup>†</sup> and p<sup>†</sup>nn<sup>†</sup> InP homojunction solar cell configurations appear capable of yielding beginning-of-life (BOL) 1AMO, 25°C efficiency of slightly It should be noted that our near-optimum designs use over 22.5%. realistically achievable values of 4% grid shadowing, a two-layer AR coating of  $ZnS/MgF_2$ , front SRV values of  $10^4$  cm/s on top of th  $n^+$  emitter

and  $10^3$  cm/s on top of the p $^+$  emitter. The thickness of and doping in each region also have realistic values. The primary requirement to achieve the efficiency of 22.5% is that the indirect or Hall-Shockley-Reed minority carrier lifetime coefficients for n-type and p-type InP be ten times their values found from the solar cell Spire6.

With the materials technology of InP constantly improving, we expect this to be achievable in the very near future, if it is already not so.

- 2. For both the  $n^{\dagger}pp^{\dagger}$  and  $p^{\dagger}nn^{\dagger}$  configurations, the largest fraction of the photocurrent comes from the p-type region  $p^{\dagger}$  emitter in the  $p^{\dagger}nn^{\dagger}$  cell and p-type bases in the  $n^{\dagger}pp^{\dagger}$  cell. Hence the performance of the cell is most sensitive to the geometrical and material parameters of the p-type region in each configuration.
- 3. The maximum efficiencies of the two configurations being nearly equal, the choice of configuration  $(n^tpp^t \text{ or } p^tnn^t)$  is dictated by other considerations such as ease and cost of fabrication and radiation tolerance under a specific radiation environment.

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